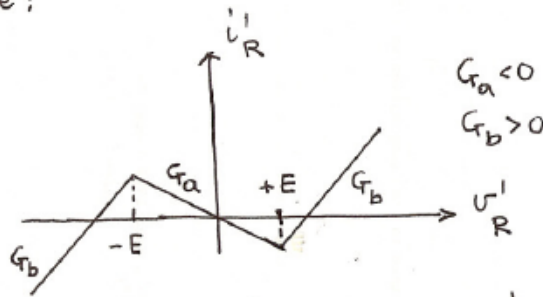
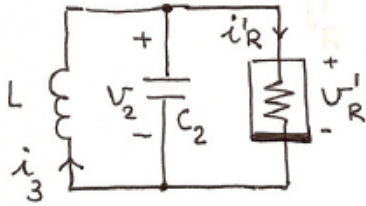


# Nonlinear state equation formulation

## Example # 1

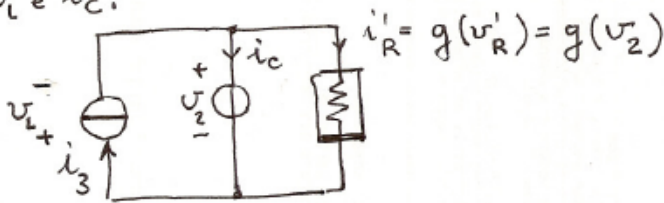
Si scrivano le equazioni di stato per il circuito seguente:



$$i'_R = G_b v'_R + \frac{1}{2} (|v'_R + E| - |v'_R - E|) (G_a - G_b)$$

Assumo \$v\_2\$ e \$i\_3\$ come variabili di stato

Sostituisco il condensatore con un generatore di tensione e l'induttore con un generatore di corrente e calcolo le grandezze "conjugate" \$v\_L\$ e \$i\_C\$:



$$v_L = -v_2 \rightarrow L \frac{di_3}{dt} = -v_2 ; \frac{di_3}{dt} = -\frac{1}{L} v_2$$

$$i_C = i_3 - i'_R \rightarrow C_2 \frac{dv_2}{dt} = +i_3 - g(v_2); \frac{dv_2}{dt} = -\frac{1}{C_2} i_3 - \frac{1}{C_2} g(v_2)$$

In definitiva le eq. di stato sono:

$$\begin{cases} \frac{dv_2}{dt} = -\frac{1}{C_2} g(v_2) + \frac{1}{C_2} i_3 \\ \frac{di_3}{dt} = -\frac{1}{L} v_2 \end{cases}$$

Example # 2 (Hasler-Neiryck, p. 113)

Let us consider the Wien-bridge oscillator of figure 2.56 (vol. VIII, subsec. 5.3.5). The associated resistive circuit is shown in figure 2.57. According to (2.146), the currents  $i_1$  and  $i_2$  must be expressed as a function of the voltages  $v_{c1}$  and  $v_{c2}$ . If the two-port were linear, the admittance matrix should be calculated.

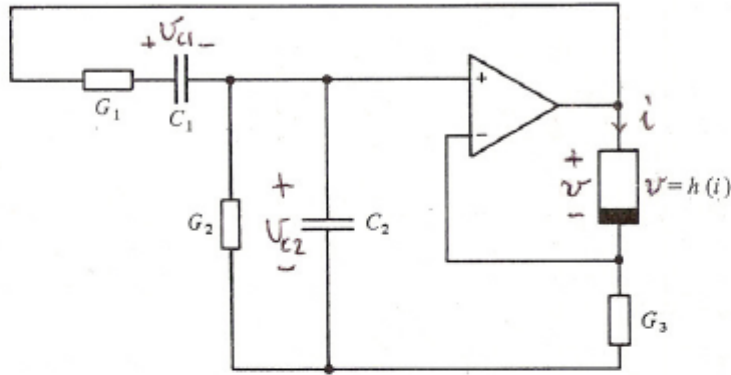


Fig. 2.56

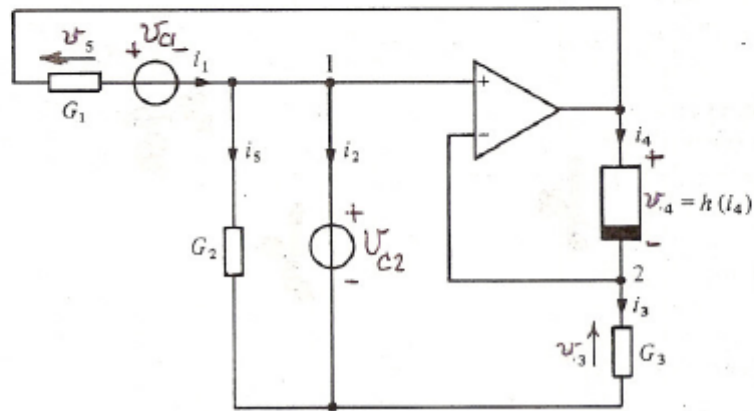


Fig. 2.57

Ci noti che  $v_3 = v_{c2}$  e che  $i_4 = i_3$

$$\text{Quindi } v_4 = h(i_4) = h(v_{c2} G_3)$$

Ora posso calcolare  $i_1$ :

$$\begin{aligned} i_1 &= \left[ (v_3 + v_4) - (v_{c1} + v_{c2}) \right] G_1 = \\ &= \left[ \cancel{v_{c2}} + h(v_{c2} G_3) - v_{c1} - \cancel{v_{c2}} \right] G_1 = \\ &= -v_{c1} G_1 + G_1 h(v_{c2} G_3) \end{aligned}$$

Ma  $i_1 = C_1 \frac{dv_{c1}}{dt}$  e quindi:

$$\frac{dv_{c1}}{dt} = -\frac{1}{R_1 C_1} v_{c1} + \frac{1}{R_1 C_1} h(v_{c2} G_3)$$

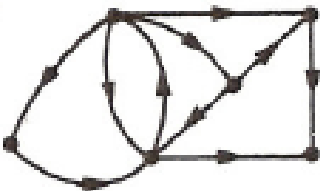
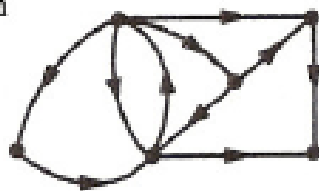

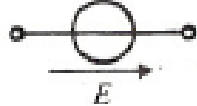


$$\text{Infine } i_2 = i_1 - i_5 = i_1 - v_{c2} G_2 =$$

$$= -v_{c1} G_1 - v_{c2} G_2 + G_1 h(v_{c2} G_3)$$

Le eq. di stato sono:

$$\begin{cases} \frac{dv_{c1}}{dt} = -\frac{1}{R_1 C_1} v_{c1} + \frac{1}{R_1 C_1} h(v_{c2} G_3) \\ \frac{dv_{c2}}{dt} = -\frac{1}{R_1 C_2} v_{c1} - \frac{1}{R_2 C_2} v_{c2} + \frac{1}{R_1 C_2} h(v_{c2} G_3) \end{cases}$$

Nonlinear state equation formulation: step 1 (Hasler-Neiryck, p. 112)

Original Circuit	Associated Resistive Circuit
<p>Graph</p> 	<p>Graph</p>  <p style="text-align: center;">← identical →</p>
	
	

Nonlinear state equation formulation: step 2 (CDK, p. 405)

*Capacitor*

1. If the capacitor is *voltage-controlled*, i.e.,

$$q_{Cj} = \hat{q}_{Cj}(v_{Cj}) \quad (4.14a)$$

then choose *capacitor voltage*  $v_{Cj}$  as the state variable.

2. If the capacitor is *charge-controlled*, i.e.,

$$v_{Cj} = \hat{v}_{Cj}(q_{Cj}) \quad (4.14b)$$

then choose *capacitor charge*  $q_{Cj}$  as the state variable.

*Inductor*

1. If the inductor is *current-controlled*, i.e.,

$$\phi_{Lj} = \hat{\phi}_{Lj}(i_{Lj}) \quad (4.15a)$$

then choose *inductor current*  $i_{Lj}$  as the state variable.

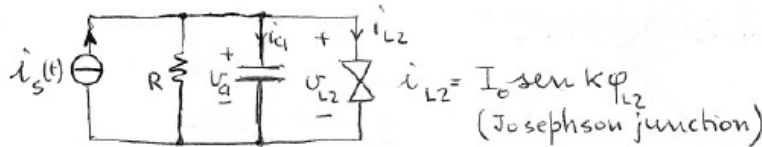
2. If the inductor is *flux-controlled*, i.e.,

$$i_{Lj} = \hat{i}_{Lj}(\phi_{Lj}) \quad (4.15b)$$

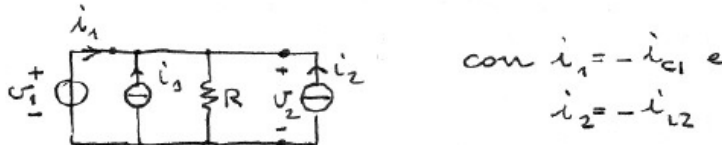
then choose *inductor flux*  $\phi_{Lj}$  as the state variable.

### Example # 3

Si consideri questo nuovo esempio: (CDK, p. 401)



Assumo  $v_{C_1}$  e  $\varphi_{L_2}$  come variabili di stato.  
 Creo il circuito resistivo associato:



con  $i_1 = -i_{C_1}$  e  
 $i_2 = -i_{L_2}$

Devo calcolare  $i_1$  e  $v_2$  in funzione di  $v_1$  e  $i_2$

$$\begin{cases} i_1 = -i_3 + C_1 \frac{dv_1}{dt} - i_2 \\ v_2 = v_1 \end{cases} \quad \text{ma } i_1 = C_1 \frac{dv_1}{dt} \text{ e } v_2 = d\varphi_{L_2}/dt.$$

Quindi ho:

$$\begin{cases} \frac{d v_{C_1}}{dt} = -\frac{v_{C_1}}{R C_1} - \frac{1}{C_1} I_0 \sin k\varphi_{L_2} + \frac{1}{C_1} i_3(t) \\ d\varphi_{L_2}/dt = v_{C_1} \end{cases}$$

### General remarks (CDK, p. 364 and 400)

1.

There are two important reasons for writing state equations. *First*, all properly modeled circuits have a well-defined state equation. *Second*, most analytic and numerical methods for solving *nonlinear* differential equations are formulated in terms of the above standard form.

Note that to qualify as a state equation,  $\dot{x}_1$  and  $\dot{x}_2$  must appear on the left-hand side, and only  $x_1$  and  $x_2$  can appear on the right-hand side, in addition to possibly the independent time variable  $t$ .

In the special case where the circuit contains only time-invariant elements and dc independent sources, the time variable does not appear explicitly. In this case, Eq. (4.1) reduces to

$$\begin{array}{l} \text{Autonomous} \\ \text{state equation} \end{array} \quad \begin{array}{l} \dot{x}_1 = f_1(x_1, x_2) \\ \dot{x}_2 = f_2(x_1, x_2) \end{array} \quad \text{or} \quad \dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}) \quad (4.2)$$

Equation (4.2) is usually called an *autonomous* state equation in the literature.<sup>19</sup> Consequently, dynamic circuits containing only (linear) time-invariant elements and dc sources are called *autonomous circuits*.

2.

#### 6.1.1.3 Non-autonomous dynamical systems

A non-autonomous  $n$ -dimensional continuous-time dynamical system may be transformed to an  $(n + 1)$ -dimensional *autonomous* system by appending time as an additional state variable and writing

$$\begin{aligned} \dot{\mathbf{X}}(t) &= \mathbf{F}(\mathbf{X}(t), X_{n+1}(t)) \\ \dot{X}_{n+1}(t) &= 1 \end{aligned} \quad (5)$$